Effect of Age-Related Human Lens Sutures Growth on Its Fluid Dynamics

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PURPOSE. Age-related nuclear cataract is the opacification of the clear ocular lens due to oxidative damage as we age, and is the leading cause of blindness in the world. A lack of antioxidant supply to the core of ever-growing ocular lens could contribute to the cause of this condition. In this project, a computational model was developed to study the sutural fluid inflow of the aging human lens.

METHODS. Three different SOLIDWORKS computational fluid dynamics models of the human lens (7 years old; 28 years old; 46 years old) were created, based on available literature data. The fluid dynamics of the lens sutures were modelled using the Stokes flow equations, combined with realistic physiological boundary conditions and embedded in COMSOL Multiphysics.

RESULTS. The flow rate, volume, and flow rate per volume of fluid entering the aging lens were examined, and all increased over the 40 years modelled. However, while the volume of the lens grew by ~500% and the flow rate increased by ~100%, the flow rate per volume increased only by very moderate ~38%.

CONCLUSIONS. Here, sutural information from humans of 7 to 46 years of age was obtained. In this modelled age range, an increase of flow rate per volume was observed, albeit at very slow rate. We hypothesize that with even further increasing age (60+ years old), the lens volume growth would outpace its flow rate increases, which would eventually lead to malnutrition of the lens nucleus and onset of cataracts.

Keywords: age-related cataract, sutural inflow, finite element modelling, lens changes in aging
complicated as new branches are formed. Several different computer models in the form of cylindrical map projections (CMP) and computer aided design (CAD) had been used to describe the process of sutures growth. However, these models were generic and not representative of true aging process in humans.

In this paper, we have used clinical data to create representative computer models of human lens growth and increased complexity of sutural geometry. We then investigated the effects of these changes on water and solute influx rates at different stages of human life. It should be noted that computational modelling of a complex tissue with disruptive geometrical features, like the lens and its sutures, is a step-by-step process. The microcirculation model has been developed and optimized for over decades now, and it still does not include an accurate representation of the sutures. To fully implement the sutures, in this paper the geometry from clinical images has been obtained, representative computer meshes were created, appropriate fluid dynamics equations have been applied, and the sutural model is computationally solved, in isolation. The next step of this research would be to “connect” the computationally stable model of the sutures, with the continuum model of microcirculation, through appropriate boundary conditions selection, on both meshes.

By perfecting anatomically and physiologically accurate computational models of the human lens, we can aim to understand and predict the changes of the lens associated with aging, in its geometry, its fluid dynamics and consequently its nutrients influx. This knowledge will be used to increase our understanding of the onset of lenticular pathologies, such as age-related nuclear cataracts, and presbyopia.

METHODS

To create a fully functional fluid dynamics model of the human lens, capable of capturing its fluid and solute fluxes, several steps were followed.

Creating Realistic Sutural Geometry in 3D

In order to create anatomically accurate models of human lens sutures, it was essential to extract these geometries from clinical data sets. However, human lens sutures are optically evolved to be transparent and minimally disruptive to our vision; hence imaging them in a healthy lens proved to be extremely difficult. Sutural cataract, however, is a pathology where the sutural branches become opaque. We obtained images of three sutural cataract cases at three different ages.

In humans, the posterior sutural branches are 180 degrees out of phase with the anterior sutures and they are located at the posterior pole. These sutural branches were difficult to see in our images, so they were approximated by examining and rotating the respective anterior suture (Fig. 2). The sutural branches were initially modelled with a constant width and abrupt edges. Design tools on SOLIDWORKS (SolidWorks Corporation, Concord, MA, USA) were then used to make the edges of the sutures, as shown in Figure 2. The final dimensions for the sutural branches were 0.6 mm wide, 1.5 mm long and all three branches centred around a 0.1-mm diameter circle. The anterior sutures formed an upright Yshape with the sutural branches spaced 120 degrees apart. The posterior sutures were also centred around a 0.1-mm diameter circle; however, they formed an inverted Yshape with the branches also spaced 120 degrees apart. The branches of the original “Y” sutures were created manually and using the
design tool of SOLIDWORKS, to visually match the clinical images (Fig. 2).

Geometrical Model of the Lens

The sutural models of different ages had to be embodied in a full model of the lens of the matching age. The overall dimension of the lens was taken from literature1,2 and Table 1. It was assumed that the lenses are rotationally symmetric about the visual axis, and the dimensions of the core and the inner cortex can be determined by a ratio to the lens’ overall dimension. The SOLIDWORKS sketch tool was used to create a two-dimensional projection of the core, the inner cortex and the outer cortex, respectively. A revolved structure with these projections with an axis of revolution of 360° were then created to form the solid structures.

It was decided to separate the lens into three different regions of outer cortex, inner cortex, and the core based on previous literature.1,11,19,20 The product of this design is regions of outer cortex, inner cortex, and the core based on previous literature.11,19,20 The product of this design is created to form the solid structures.

As the lens grows with age, its thickness increases at linear rates ranging from 0.013 to 0.025 mm/year in adults.6,7 Since the growth of the lens is not at a constant rate, the dimensions of the lens at different ages cannot readily be predicted. The lens dimensions were obtained from an in vivo magnetic resonance imaging (MRI) study on healthy and diabetic participants, from which the former data set was selected.21 The dimensions for both the 28- and 46-year-old lens were based on the control groups in a study about the lens shape and refractive index distribution in type 1 diabetes. There was no available data for the dimensions of a 7-year-old lens. The lens dimensions were instead determined through interpolation on MATLAB (Mathworks, Natick, MA, USA). Interpolation requires information about the trend on either side of the desired value and the final results are summarized (Table 1) and shown (Fig. 3).

This model was then used to solve the fluid dynamics of the sutures at different stages of human life.

Fluid Dynamics Model of the Sutures

COMSOL Multiphysics (COMSOL, Inc., Palo Alto, CA, USA) was used to model the fluid dynamics of the sutural model that was created in SOLIDWORKS. In the eye, the lens is submerged anteriorly in the aqueous humour in the anterior chamber, and posteriorly in the vitreous humour in the vitreous cavity. The aqueous humour is less viscous than the vitreous humour. To model this phenomenon, the fluid properties and the typical fluid velocity of the aqueous and vitreous humour were used (Table 2).9,10 In this instance of applying the boundary conditions, we determined the general inflow velocity magnitude to be 2e-4 and 6e-3 mm/s at the surfaces of the anterior and posterior sutures, respectively. These conditions were applied with a “normal to surface” condition selected within COMSOL Multiphysics programming platform. The modelling software then correctly applied the boundary conditions, with respect to the geometrical structure of the model. Thus, the velocity boundary condition is always normal to the surface and the user did not have to create an explicit set of boundary conditions to supply to the software.

The fluid dynamics of the lens and in turn the sutures can be modelled by a simplified version of the Navier-Stokes equations.22–24 It assumed the fluid in the lens is an incompressible Newtonian fluid with a spatially constant viscosity at steady state. The second assumption is that the fluid flow in the lens is a creeping or low-Reynolds number flow with negligible turbulence.8 From these assumptions, the fluid in the lens is modelled by a simplified version of the Navier-Stokes equations (Equation 1 and Equation 2).

\[ \nabla \cdot u = 0 \]  

\[ -\nabla p + \mu \nabla^2 u + f = 0 \]  

Here, \( u \) is the velocity (m/s), \( p \) is the hydrostatic pressure (N/m²), \( \mu \) is the dynamic viscosity (N · s/m²), and \( f \) is the body force per unit mass (N/kg) acting on the fluid. The boundary conditions of the bulk fluid movement model were determined from literature. Fluid entered the anterior and posterior lens with velocities of 2 × 10⁻⁴ mm/s² and 6 × 10⁻³ mm/s, respectively, which mimics the typical flow velocities in the aqueous and vitreous humour, respectively.

A notable difference between this implementation and previous models4,27,28 is that there exists a pressure difference between the anterior and posterior lens.9,14 This difference in pressure was calculated by a MATLAB script, which utilises the ratio between the intraocular pressure (IOP) of the anterior and posterior chambers and the properties of the adjacent humour1,2 and Table 1. The overall ratio between the intraocular pressure (IOP) of the anterior and posterior chambers was not known and hence was determined from literature1,2 and Table 1. The overall pressure difference calculated from the MATLAB script was used to model the fluid dynamics of the sutures in both the anterior and posterior chambers.

| Table 1. Dimensions of the Human Lenses Including Interpolated Values for the 7-Year-Old |

<table>
<thead>
<tr>
<th>Age of Lens, y</th>
<th>Equatorial Length Diameter, mm</th>
<th>Anterior Axial Thickness, mm</th>
<th>Posterior Axial Thickness, mm</th>
</tr>
</thead>
<tbody>
<tr>
<td>0</td>
<td>6.00</td>
<td>1.10</td>
<td>1.40</td>
</tr>
<tr>
<td>7</td>
<td>7.16</td>
<td>0.98</td>
<td>1.66</td>
</tr>
<tr>
<td>28</td>
<td>9.32</td>
<td>1.04</td>
<td>2.34</td>
</tr>
<tr>
<td>46</td>
<td>9.61</td>
<td>1.57</td>
<td>2.80</td>
</tr>
</tbody>
</table>

| Table 2. Fluid Properties in the Anterior and Posterior Chambers of the Eye |

<table>
<thead>
<tr>
<th>Fluid Properties</th>
<th>Density ( \rho ) (kg/m³)</th>
<th>Dynamic Viscosity ( \mu ) (Pa · s)</th>
<th>Fluid Velocity ( u ) (mm/s)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Aqueous humour</td>
<td>1000</td>
<td>1</td>
<td>2 × 10⁻⁴</td>
</tr>
<tr>
<td>Vitreous humour</td>
<td>1000</td>
<td>0.7</td>
<td>6 × 10⁻³</td>
</tr>
</tbody>
</table>

**Figure 3.** Three-dimensional model of the human lens showing the lens geometry. SOLIDWORKS models of the lens sutures showing the difference in sutural complexity (from left to right: 7 years old, 28 years old, and 46 years old) in (A) axial and (B) coronal view. In (A) and for all the models, the anterior side is up, with core and posterior sides labelled accordingly. In (B) and for all the models the anterior side is facing the reader, while the equator is around the edge of the figure.
chamber. IOP has a wide normal range in humans (10–21 mm Hg). However, since the sutural model needed a single value as boundary condition, we chose the typical IOP for human to be 16 mm Hg, the pressure of the vitreous cavity was set to be 20.5 mm Hg. This pressure gradient within the suture can be calculated by Equation 3 and as shown by the blue arrows in Figure 4.

$$p(x, y, z) = -\rho_{surf} \left( \sqrt{x^2 + y^2 + z^2} \right)^2 + \rho_{surf}$$ (3)

Here $\rho_{surf}$ is the pressure of the surface of the lens, $\sqrt{x^2 + y^2 + z^2}$ is the radius of the lens and $b$ is the height of the anterior and posterior lens, respectively. The pressure of the centre of the lens is assumed to be 0 mm Hg, a diagrammatic view of the sutural model boundary conditions can be seen in Figure 4. The extracellular pressure of the lens is not experimentally measured yet and only intracellular pressure measurements are available. It was necessary to assume an extracellular pressure gradient, for our sutural model to be solvable. Hence, it was decided to “mirror” the measured intracellular pressure. By “mirror,” we mean low extracellular pressure where intracellular pressure is high, and high extracellular pressure where intracellular pressure is low. Hence, the “mirror” assumption implies a higher extracellular pressure at the surface and lower extracellular pressure at the core of the lens, based on observed “mirrored” intracellular distributions of electrical voltage and solute concentrations.

The 3D geometry of the sutures was discretized to have maximum element size of $2.44 \times 10^{-4}$ m, the minimum element size is $1.77 \times 10^{-5}$ m, the maximum element growth rate of 1.4, the curvature factor of 0.4, and the resolution of narrow regions of 0.7 (Fig. 4). The particular factors used in the mesh generation were default from COMSOL Multiphysics where the color bar expresses the velocity magnitude throughout the domain of interest (Fig. 5). In all the patterns, the red areas represented where the fluid was travelling with a faster velocity and blue, slower (Fig. 6).

Using data export function of COMSOL Multiphysics, the velocity of sutural models at varying ages, the velocity of the fluid at two distinct points, one in the anterior and the other in the posterior part of the lens were extracted (Fig. 4). These points were deemed to be of interest, because they are the intersection points where the end of the sutures meet the core of the lens. The positioning of points 1 and 2 at each age stage model and the magnitude of fluid velocity at point 1 and point 2 of the sutural models are listed here (Table 3).

The fluid-flow patterns were produced in the COMSOL Multiphysics where the color bar expresses the velocity magnitude at anterior and posterior surface nodes were first exported from COMSOL Multiphysics, these were subsequently summed to find the total velocity magnitude ($\vec{U}$). The surface area of the sutural outlets were then obtained in COMSOL Multiphysics ($A$) and the flowrate was calculated by multiplying the total velocity magnitude with the outlet sutural surface area ($\dot{q} = \vec{u} \cdot \vec{A}$). The total volume of the three lenses were obtained from COMSOL Multiphysics ($V$). This volume information was then used to calculate the flowrate per volume ($\dot{q} = \dot{V} / V$) (Table 4).

From these results, it appeared that the velocity of sutural fluxes increased with age. Combined with increased surface area of sutures through “branching,” the flowrate is also increased within the sutures. However, the volume of the lens ($V$) has also increased with aging, which affects the parameter flowrate per volume ($\dot{q}$). The age-related changes of these parameters are plotted here (Fig. 6).

It was very interesting to observe (Fig. 6) that flowrate and volume grow at about the same rate. This concludes that the flowrate per volume ($\dot{q}$) is relatively constant with aging. In the absence of experimental data, we can only speculate that this observation might have some implication for understanding the process of aging in the human lens.
CONCLUSIONS

The human lens grows by adding new fibre cell layers at the periphery, which results in increase in thickness and diameter with age in a nonlinear fashion.\(^{11,34–38}\) This process is accompanied by compaction of fibre cells, especially in the core and inner cortex of the lens, overall flattening of the lens and branching of the originally Y-shaped sutures into "shape ultrastructure.\(^{10,39–41}\) Although complex in nature, the main outcome of this process is for the core of the lens to buried deeper inside the tissue and becoming less accessible by eye’s humours. This in turn translates to reduced supply of nutrients (especially antioxidants) to the lens core with advancing age, accumulated oxidative damage, and ultimately onset of age-related nuclear cataract. However, most humans can live without significant cataract for six decades, and sometimes much longer. We believe that sutures “branching” with age, is an evolutionary compensatory mechanism that could to some extent improves the lens core accessibility.

Here, clinical images of sutural cataract were used to create 3D realistic models of the sutures. These models were then combined with realistic geometries of the lens volume at different ages, based on published measurements. Finally, fluid dynamics of the sutures were modelled using simplified Navier-Stokes equations and published boundary conditions. Overall, an increase in velocity of sutural fluxes was with aging of our model. This increase, combined with larger sutural surface area through “branching” led to higher sutural flowrates, under employed modelling conditions here. However, the flowrate per volume seemed to be relatively constant with age. It should be noted that it is very difficult to choose an average shape and dimension of a human lens, at a certain age. This is due to ethnicity-related eye-shape factor, varying refractive errors, accommodation capacities, and potential presence of cataracts in an age-matched population. Comprehensive clinical ocular and lenticular biometric studies are needed to establish a more representative model of changing human lens and sutures in aging.

Another limitation of this study was that it had to use available sutural cataract data sets, to create a representative

| TABLE 4. The Sum of the Velocity (\(\sum U\)), Sutures Surface Area (A), Flow Rate (q), Volume (V), and Flowrate per Volume Ratio (\(\dot{q}\)) for the Sutural Models |
|---|---|---|---|---|---|
| Age, y | \(\sum U\), m/s | A (m²) | q (m³/s) | V (m³) | \(\dot{q}\) (s⁻¹) |
| 7 | 986.23 | 1.44E-05 | 0.014 | 7.01E-08 | 203233.9 |
| 28 | 1325.07 | 2.33E-05 | 0.031 | 1.52E-07 | 202325.5 |
| 46 | 1908.74 | 3.02E-05 | 0.058 | 2.06E-07 | 279589.3 |

**Figure 5.** Fluid velocity pattern of (A) 7 years old, (B) 28 years old, and (C) 46 years old. The units on the color bar are in mm/s.

**Figure 6.** Graph of the change in volume (blue), flowrate (orange), and flowrate per volume ratio (green).
model of the suture’s geometry. This meant that the oldest lens modelled here was 46 years old. Currently, several imaging modalities are being investigated in our lab to visualize the sutural patterns of healthy lenses. By imaging larger number of participants over a more extended lifetime period, the scope of this project will be expanded and the hypothesis of flowrate per volume decline at later ages can be examined.

The oldest lens in this project was 46 years old. It is known that volume growth is a function of radius-cube ($r^3$), while sutural surface area increase is related to radius-square ($r^2$). Since the sutural flow rate changes with aging in humans have not been measured experimentally, using the results of our study here, we can speculate that the flowrate per volume might then begin to decline, leading to reduced delivery of antioxidants to the central region of the lens, leading to onset of age-related nuclear cataract.

The presented work here, is an isolated model of the lens sutures, and is not “connected” to a model of the rest of the lens. However, geometrically, the sutural model is the only missing piece of the established microcirculation model. The current form of the microcirculation implementation is a bi-domain continuum model. As the name suggests, the bi-domain model is designed to work as a non-aqueous radial continuum model, by design, includes predefined ratios locally varying ratios of intracellular and extracellular spaces. Each element of the bi-domain continuum model, by design, includes predefined ratios locally varying ratios of intracellular and extracellular spaces of the lens. The bi-domain continuum model then tries to simulate the “net effect” of fluid dynamics of those domains. The bi-domain continuum model is based on the symmetrical nature of the lens. As a result, the asymmetrical structure of the sutures, especially in primates are not currently captured. Hence, the disruptive geometry, fluid dynamics, and age-related changes of sutures of the lens are not currently captured by the bi-domain model. Our current work is a step toward a comprehensive model of the lens microcirculation, by capturing the asymmetrical nature of the lens sutures, and its nonlinear changes with age. We are improving our model toward a comprehensive computational predictive tool, “connecting” the sutural and microcirculation models, so that clinicians could “estimate” an age of cataract onset, based on individual patient data and accurate fluid dynamics modelling.

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References


